## Custom Solutions <br> (8) <br> Q Inspection <br> Total Metrology Solutions

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## Total Metrology Solutions

MSI Viking is your single-source comprehensive provider of precision metrology systems, services, and custom engineered solutions. We represent more than 100 of the world's leaders in precision measuring instruments, gaging, and process automation. This means providing the solutions you need rather than a limited handful of options.

In addition to precision measurement product sales and support, we are a leading provider of A2LA ISO 17025 accredited lab and on-site calibration and inspection services, and repair services. Our team of experts can also deliver custom engineered solutions leveraging advanced automation and control systems, machine vision, and robotic technologies.

MSI Viking is committed to understanding your needs and providing innovative, practical, on-budget solutions. Turn to MSI Viking for the most complete range of options, answers and expertise.

Because we truly are Your Total Metrology Solution.

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## How Big is a Micron? ( $\mu \mathrm{m}$ )

$1 \mu \mathrm{~m}=1$ Millionth of 1 Meter
$1 \mu \mathrm{~m}=40$ Millionths of 1 Inch


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## Standard Reference Chart

## Standard English Terminology in Terms of an Inch

$$
\begin{gathered}
1.0=\text { One Inch } \\
\hline 0.5=\text { One half of an Inch } \\
\hline 0.100=\text { One Hundredth of an inch } \\
0.001=\text { One thousandth of an inch } \\
0.0001=\text { One ten thousandth of an inch or "a tenth" } \\
\hline 0.00001=\text { Ten Millionths of an Inch } \\
0.000001=\text { One Millionth of an Inch }
\end{gathered}
$$

Metric Terminology in Terms of a Millimeter $1.0=$ One Millimeter
$0.1=100$ Microns
$0.01=10$ Microns

$$
0.001 \text { = } 1 \text { Micron }
$$

## Common Conversion Factors

$$
\frac{1^{\prime \prime}=25.4 \mathrm{~mm}}{1 \mathrm{~mm}=.03937^{\prime \prime}}
$$

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## METRIC to INCH CONVERSION TABLE

| Metric | Inch | Metric | Inch | Metric | Inch | Metric | Inch |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.01 | 0.00039 | 0.51 | 0.02008 | 1 | 0.03937 | 51 | 2.00787 |
| 0.02 | 0.00079 | 0.52 | 0.02047 | 2 | 0.07874 | 52 | 2.04724 |
| 0.03 | 0.00118 | 0.53 | 0.02087 | 3 | 0.11811 | 53 | 2.08661 |
| 0.04 | 0.00157 | 0.54 | 0.02126 | 4 | 0.15748 | 54 | 2.12598 |
| 0.05 | 0.00197 | 0.55 | 0.02165 | 5 | 0.19685 | 55 | 2.16535 |
| 0.06 | 0.00236 | 0.56 | 0.02205 | 6 | 0.23622 | 56 | 2.20472 |
| 0.07 | 0.00276 | 0.57 | 0.02244 | 7 | 0.27559 | 57 | 2.24409 |
| 0.08 | 0.00315 | 0.58 | 0.02283 | 8 | 0.31496 | 58 | 2.28346 |
| 0.09 | 0.00354 | 0.59 | 0.02323 | 9 | 0.35433 | 59 | 2.32283 |
| 0.10 | 0.00394 | 0.6 | 0.02362 | 10 | 0.3937 | 60 | 2.3622 |
| 0.11 | 0.00433 | 0.61 | 0.02402 | 11 | 0.43307 | 61 | 2.40157 |
| 0.12 | 0.00472 | 0.62 | 0.02441 | 12 | 0.47244 | 62 | 2.44094 |
| 0.13 | 0.00512 | 0.63 | 0.0248 | 13 | 0.51181 | 63 | 2.48031 |
| 0.14 | 0.00551 | 0.64 | 0.0252 | 14 | 0.55118 | 64 | 2.51968 |
| 0.15 | 0.00591 | 0.65 | 0.02559 | 15 | 0.59055 | 65 | 2.55905 |
| 0.16 | 0.0063 | 0.66 | 0.02598 | 16 | 0.62992 | 66 | 2.59842 |
| 0.17 | 0.00669 | 0.67 | 0.02638 | 17 | 0.66929 | 67 | 2.63779 |
| 0.18 | 0.00709 | 0.68 | 0.02677 | 18 | 0.70866 | 68 | 2.67716 |
| 0.19 | 0.00748 | 0.69 | 0.02717 | 19 | 0.74803 | 69 | 2.71653 |
| 0.20 | 0.00787 | 0.7 | 0.02756 | 20 | 0.7874 | 70 | 2.7559 |
| 0.21 | 0.00827 | 0.71 | 0.02795 | 21 | 0.82677 | 71 | 2.79527 |
| 0.22 | 0.00866 | 0.72 | 0.02835 | 22 | 0.86614 | 72 | 2.83464 |
| 0.23 | 0.00906 | 0.73 | 0.02874 | 23 | 0.90551 | 73 | 2.87401 |
| 0.24 | 0.00945 | 0.74 | 0.02913 | 24 | 0.94488 | 74 | 2.91338 |
| 0.25 | 0.00984 | 0.75 | 0.02953 | 25 | 0.98425 | 75 | 2.95275 |
| 0.26 | 0.01024 | 0.76 | 0.02992 | 26 | 1.02362 | 76 | 2.99212 |
| 0.27 | 0.01063 | 0.77 | 0.03032 | 27 | 1.06299 | 77 | 3.03149 |
| 0.28 | 0.01102 | 0.78 | 0.03071 | 28 | 1.10236 | 78 | 3.07086 |
| 0.29 | 0.01142 | 0.79 | 0.0311 | 29 | 1.14173 | 79 | 3.11023 |
| 0.30 | 0.01181 | 0.8 | 0.0315 | 30 | 1.1811 | 80 | 3.1496 |
| 0.31 | 0.0122 | 0.81 | 0.03189 | 31 | 1.22047 | 81 | 3.18897 |
| 0.32 | 0.0126 | 0.82 | 0.03228 | 32 | 1.25984 | 82 | 3.22834 |
| 0.33 | 0.01299 | 0.83 | 0.03268 | 33 | 1.29921 | 83 | 3.26771 |
| 0.34 | 0.01339 | 0.84 | 0.03307 | 34 | 1.33858 | 84 | 3.30708 |
| 0.35 | 0.01378 | 0.85 | 0.03346 | 35 | 1.37795 | 85 | 3.34645 |
| 0.36 | 0.01417 | 0.86 | 0.03386 | 36 | 1.41732 | 86 | 3.38582 |
| 0.37 | 0.01457 | 0.87 | 0.03425 | 37 | 1.45669 | 87 | 3.42519 |
| 0.38 | 0.01496 | 0.88 | 0.03465 | 38 | 1.49606 | 88 | 3.46456 |
| 0.39 | 0.01535 | 0.89 | 0.03504 | 39 | 1.53543 | 89 | 3.50393 |
| 0.40 | 0.01575 | 0.90 | 0.03543 | 40 | 1.5748 | 90 | 3.5433 |
| 0.41 | 0.01614 | 0.91 | 0.03583 | 41 | 1.61417 | 91 | 3.58267 |
| 0.42 | 0.01654 | 0.92 | 0.03622 | 42 | 1.65354 | 92 | 3.62201 |
| 0.43 | 0.01693 | 0.93 | 0.03661 | 43 | 1.69291 | 93 | 3.66141 |
| 0.44 | 0.01732 | 0.94 | 0.03701 | 44 | 1.73228 | 94 | 3.70078 |
| 0.45 | 0.01772 | 0.95 | 0.0374 | 45 | 1.77165 | 95 | 3.74015 |
| 0.46 | 0.01811 | 0.96 | 0.0378 | 46 | 1.81102 | 96 | 3.77952 |
| 0.47 | 0.0185 | 0.97 | 0.03819 | 47 | 1.85039 | 97 | 3.81889 |
| 0.48 | 0.0189 | 0.98 | 0.03858 | 48 | 1.88976 | 98 | 3.85826 |
| 0.49 | 0.01929 | 0.99 | 0.03898 | 49 | 1.92913 | 99 | 3.89763 |
| 0.5 | 0.01969 | 1.00 | 0.03937 | 50 | 1.9685 | 100 | 3.937 |

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## Gagemaker's Tolerance Chart [ANSI/AMSE B89.1.5]* INCH

| Diameter Range Above-Including | XXX | XX | X | Y | Z | ZZ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .010"-.825" | .000010" | .000020" | .000040" | .000070" | .0001" | .0002" |
| .825"-1.510" | .000015" | .000030" | .000060" | .000090" | .00012" | .00024" |
| 1.510"-2.510" | .000020" | .000040" | .000080" | .00012" | .00016" | .00032" |
| 2.510"-4.510" | .000025" | .000050" | .0001" | .00015" | .0002" | .0004" |
| 4.510"-6.510" | .000033" | .000065" | .00013" | .00019" | .00025" | .0005" |
| 6.510"-9.010" | .000040" | .000080" | .00016" | .00024" | .00032" | .00064" |
| 9.010"-12.010" | .000050" | .0001" | .0002" | .0003" | .0004" | .0008" |

Gagemaker's Tolerance Chart [ANSI/AMSE B89.1.5]*

METRIC

| Diameter Range <br> Above-Including | XXX | XX | $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ | $\mathbf{Z Z}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $.254 \mathrm{~mm}-\mathbf{2 0 . 9 6 m m}$ | .00025 mm | .00051 mm | .00102 mm | .00178 mm | .00254 mm | .00508 mm |
| $\mathbf{2 0 . 9 6 \mathrm { mm } - 3 8 . 3 5 \mathrm { mm }}$ | .00038 mm | .00076 mm | .00152 mm | .00229 mm | .00305 mm | .00610 mm |
| $\mathbf{3 8 . 3 5 \mathrm { mm } - 6 3 . 7 5 \mathrm { mm }}$ | .00051 mm | .00102 mm | .00203 mm | .00305 mm | .00406 mm | .00813 mm |
| $\mathbf{6 3 . 7 5 \mathrm { mm } - 1 1 4 . 5 5 \mathrm { mm }}$ | .00064 mm | .00127 mm | .00254 mm | .00381 mm | .00508 mm | .01016 mm |
| $\mathbf{1 1 4 . 5 5 \mathrm { mm } - 1 6 5 . 3 5 \mathrm { mm }}$ | .00084 mm | .00165 mm | .00330 mm | .00483 mm | .00635 mm | .01270 mm |
| $\mathbf{1 6 5 . 3 5 \mathrm { mm } - \mathbf { 2 2 8 . 8 5 m m }}$ | .00102 mm | .00203 mm | .00406 mm | .00610 mm | .00813 mm | .01626 mm |
| $\mathbf{2 2 8 . 8 5 m m - 3 0 5 . 0 5 \mathrm { mm }}$ | .00127 mm | .00254 mm | .00508 mm | .00762 mm | .01016 mm | .02032 mm |

[^0]
## Measurement System Characterization

| Location (Average Measurement Value vs. Actual Value) |  |
| :---: | :--- |
| Stability | The ability of a measurement system to produce the same values over time when measuring the same <br> sample. |
| Accuracy | A measure of the distance between the average value of the measurement of a part and the True, certified, <br> or assigned value of a part. Also referred to as bias. |
| Linearity | The consistency of accuracy (bias) over the range of measurement; a slope of one (unity) between mea- <br> sured and true value is perfect. |
| Variation (Spread of Measurement Values - Precision) |  |$|$| Repeatability | The consistency of a single appraiser to measure the same part multiple times with the same measure- <br> ment system; it is related to the standard deviation of the measured values. |
| :--- | :--- |
| Reproducibility | Assesses whether different appraisers can measure the same part/sample with the same measurement <br> device and get the same value. |
| Resolution | The ability of a measurement system to discriminate between measurement values. The consistency <br> of different appraisers in measuring the same part with the same measurement system; it is related to <br> standard deviation of the distribution of appraiser averages. |

The diagram below illustrates the difference between the terms "Accuracy" and "Precision". Efforts to improve measurement system quality are aimed at improving both accuracy and precision.


## Requirements

Following are general requirements of all capable measurement systems:

- Statistical stability over time.
- Variability small compared to the process variability.
- Variability small compared to the specification limits (tolerance).
-The resolution, or discrimination of the measurement device must be small relative to the smaller of either the specification tolerance or the process spread (variation). As a rule of thumb, the measurement system should have resolution of at least $1 / 10$ th the smaller of either the specification tolerance or the process spread. If the resolution is not fine enough, process variability will not be recognized by the measurement system, thus blunting its effectiveness.


## Total Metrology Solutions

## Basic Surface Finish



| PROFILE |  |
| :---: | :--- |
| Pt | Sum of Height of the largest profile peak height and largest profile valley in a evaluation length |
| Pa | Profile average arithmetic average of absolute values of the roughness profile ordinates |
| Pv | Depth of the lowest profile valley of the Profile curve in one sampling length |
| Pp | Height of the highest profile peak of the Profile curve in one sampling length |
| PSm* | Mean Width Of Profile Elements arithmetic mean value of the widths of profile elements of the Profile |
| Wt | Sum of Height of the largest Waviness profile peak height and largest Waviness valley in the evaluation <br> length |
| Wp | Largest waviness profile peak in a sampling length |
| Wa | Waviness Average arithmetic average of absolute values of the waviness profile ordinates |
| Wsm | Mean Width Of Waviness Profile Elements arithmetic mean value of widths of waviness profile elements <br> and waviness profile |
| Wq* | Root mean square average of the waviness profile ordinates |
| Ra | Roughness average arithmetic average of absolute values of the roughness profile ordinates |
| Rz | Single Roughness Depth vertical distance between the highest peak and deepest valley within a sampling <br> length |
| Rmax | Maximum Roughness Depth largest single roughness depth within evaluation length <br> RsmMean width of profile elements arithmetic mean value of widths of profile elements and roughness <br> profile |
| Rq (RMS)* | Root mean square average of the roughness profile ordinates |

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Torque Measurement

| IN-OZ | G-CM | IN-LB | FT-LB | KG-M | N-M |
| :---: | ---: | ---: | ---: | ---: | ---: |
| $\mathbf{4 8}$ | 3456 | 3 | 0.25 | 0.03458 | 0.339 |
| $\mathbf{1 9 2}$ | 13830 | 12 | 1 | 0.1383 | 1.356 |
| $\mathbf{8 0 0}$ | 57600 | 50 | 4.167 | 0.5763 | 5.65 |
| $\mathbf{1 6 0 0}$ | 115200 | 100 | 8.334 | 1.1526 | 11.3 |
| $\mathbf{3 2 0 0}$ | 230400 | 200 | 16.668 | 2.3052 | 22.6 |

Torque Conversion Multipliers

|  | IN-OZ | G-CM | IN-LB | FT-LB | KG-M | N-M |
| :---: | :---: | ---: | :---: | :---: | ---: | ---: |
| in-oz | 1 | 72.01 | 0.0625 | 0.005208 | 0.0007203 | 0.007063 |
| g-cm | 0.01389 | 1 | 0.000868 | 0.00007233 | 0.00001 | 0.00009808 |
| in-lb | 16 | 1152 | 1 | 0.08333 | 0.01153 | 0.113 |
| $\mathrm{ft}-\mathrm{lb}$ | 192 | 3456 | 12 | 1 | 0.1383 | 1.356 |
| $\mathrm{~kg}-\mathrm{m}$ | 1388 | 99960 | 86.77 | 7.231 | 1 | 9.805 |
| $\mathrm{n}-\mathrm{m}$ | 141.6 | 10200 | 8.85 | 0.7375 | 0.102 | 1 |


| Force Measurement |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | :---: |
| 0ZF | GF | LBF | KGF | N |  |
| $\mathbf{1 6}$ | 453.6 | 1 | 0.4536 | 4.448 |  |
| $\mathbf{8 0}$ | 2268 | 5 | 2.268 | 22.24 |  |
| $\mathbf{1 6 0}$ | 4536 | 10 | 4.536 | 44.48 |  |
| $\mathbf{4 0 0}$ | 11340 | 25 | 11.34 | 111.2 |  |
| $\mathbf{8 0 0}$ | 22680 | 50 | 22.68 | 222.4 |  |
| $\mathbf{1 6 0 0}$ | 45360 | 100 | 45.36 | 444.8 |  |
| $\mathbf{3 2 0 0}$ | 20720 | 200 | 90.72 | 889.6 |  |
| $\mathbf{8 0 0 0}$ | 226800 | 1000 | 226.8 | 2224 |  |
| $\mathbf{1 6 0 0 0}$ | 453600 | 453.6 | 4448 |  |  |


| Force Conversion Multipliers |  |  |  |  |  |  |
| :---: | ---: | ---: | :---: | ---: | ---: | :---: |
|  | OZF |  | GF | LBF | KGF |  |
| OZF | 1 | 28.35 | 0.0625 | 0.02835 | 0.278 |  |
| GF | 0.03527 | 1 | 0.002205 | 0.001 | 0.009806 |  |
| LBF | 16 | 453.6 | 1 | 0.4536 | 4.448 |  |
| KGF | 35.27 | 1000 | 2.205 | 1 | 9.806 |  |
| N | 3.597 | 102 | 0.2248 | 0.102 | 1 |  |

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## Form Parameter Tolerances


$\square$
Straightness, ISO 1101
The tolerance zone is limited in the measuring plane by two parallel straight lines a distance $t$ apart.


Cylindricity, ISO 1101
The tolerance zone is limited by two coaxial cylinders a distance $t$ apart.


The tolerance zone is limited by two parallel planes a distance $t$ apart and inclined at the specified angle to the surface.


Parallelism, ISO 1101
The tolerance zone is limited in the measuring plane by two straight lines a distance $t$ apart and parallel to the datum.
The tolerance zone is limited by two parallel planes a distance $t$ apart and symmetrically disposed to the median plane with respect to the datum axis or datum plane.


Concentricity/Coaxiality, ISO 1101
The tolerance zone is limited by a cylinder of diameter $t$, the axis of which coincides with the datum axis.


If the tolerance value is preceded by the sign, the tolerance zone is limited by a cylinder of diameter $t$, the axis of which is theoretically in the exact position of the toleranced line.


$\boxed{4}$Total run-out, ISO 1101

The tolerance zone is limited by two parallel planes a distance $t$ apart and perpendicular to the datum axis.


Profile any surface, ISO 1101
The tolerance zone is limited by two surfaces enveloping spheres of diameter $t$, the centres of which are situated on a surface having the true geometrical form.

|  |  |  | səse9 əlqon səuə60｜er |  |  |  |  |  | s｜ctrew ग！seg |  | s！erəw uonssued |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\underset{\text { ZOL }}{\substack{101.69 Z \\ \text { wni\|lgon }}}$ |  | $960^{\circ} \angle 9 Z$ แก！யшəョ U」 001 |  |  | $\begin{gathered} 0 \angle 0 \angle \nabla z \\ \text { wn!\|әy10g } \\ \text { Y\& } \end{gathered}$ |  | 190 ®ャて un！̣！uauv U $\forall$ G6 | $+90^{\circ} \downarrow \triangleright 乙$ un！uopnld nd 76 | $8 \pm 0^{\circ} \angle \varepsilon \tau$ mn！̣unden dN $\varepsilon 6$ | 620＇8ะて un！̣ue»n |  | 8\＆0＇Z६て யก！̣OL1 41 06 | 8てO L LZて un！u！！！ヤV つV 68 | səฺ．ฺ әр！u！̣｜ | ssew әu | $\begin{aligned} & \text { enoory } \\ & \text { eN } \end{aligned}$ |
|  |  | † 86.891 un！｜｜nप1 W」 69 | 6乌で 191 แก！ 9 －ヨ <br> コヨ <br> 89 |  |  | GZ6．891 un！̣ıə $\qquad$ |  |  | $\begin{aligned} & \substack{\text { 9ع.os! } \\ \text { mпиeues } \\ \text { UUS }} \end{aligned}$ |  |  |  | 9110カー แก！ฺว $\qquad$ 89 |  | รəฺฆร әр！иециие 7 | $109$ | $u \kappa s$ <br> sequinN ग！யolv |
| umouyun แn！ŋoounun onn 8LL | $\underset{\text { LLL }}{\substack{\text { umouyun } \\ \text { unndasunun }}}$ | $\begin{gathered} \substack{[86 z] \\ \text { un!uоел!7 } \\ \Lambda 7_{91 L}} \end{gathered}$ | un！uagdunun dn Sレレ |  | umouyun wn！̣цunun $7 \cap \bigcap_{\varepsilon น}$ |  |  |  | $\mathrm{HW}_{601}^{\substack{[89 z] \\ \text { unuoupow }}}$ | $\underset{801}{\substack{[69 z] \\ \text { ungsesen }}}$ | $\begin{gathered} \begin{array}{l} \text { [ngz] } \\ \text { unnuog } \\ 48 \end{array} \\ \text { LOL } \end{gathered}$ |  | $\begin{gathered} \substack{\text { Lz92] } \\ \text { un!uqna } \\ \text { Q@ }} \end{gathered}$ |  | ع0l－68 | 9Z0＇9ZZ wnipey ey 88 |  mi！̣ues」」」 $\angle 8$ |
| $\begin{aligned} & \begin{array}{l} 810 \text { zzz } \\ \text { uopey } \\ \text { UC } \\ 98 \end{array} \end{aligned}$ |  | ［286．802］ un！uolod <br> Od <br> ヤ8 | 086．802 <br> чınus！̣a |  | モ8どャロて un！｜｜еч⿺ |  | L96． 96 plos $\mathrm{n} \forall$ 62 | 980．961 minulleld <br> $1-1$ 82 |  | をて＇061 muluso SO 92 | LOZ＇981 un！uәபप्ன əy GL | $78 \cdot \varepsilon 81$ uə！s6un」 <br> M †L | $8 \div 6.081$ unjelues E $\perp$ $\varepsilon L$ | 678．8L1 سn！ufer H ZL | IL－LS | 8てモ゙ $\llcorner$ に unlueg eg 9 G | G06てと1 uniseo $\qquad$ sg |
|  |  |  | $\mathrm{qS}_{\text {Ls }}^{\substack{09 \cdot L \cdot L L \\ \text { Ruouluy }}}$ | $\underbrace{1+2814}_{0 \mathrm{~S}}$ | 818ナレト un！̣pu UI 67 | ルーがてい un！upes $\mathrm{pO}$ <br> 8t |  | で901 Pd 97 | $906^{\prime}$ ZOL un！pouy पУ St | $\underbrace{\substack{\text { uniterniny } \\ \text { ny }}}_{t \rightarrow}$ |  |  | 906 て6 wn！qo！ qN 17 |  | 906.88 سn！Ill $6 \varepsilon$ | $\begin{gathered} \begin{array}{c} \text { z9. } 28 \\ \text { winuons } \\ 1 S_{8} \end{array} \\ 8 \end{gathered}$ |  |
|  |  | $\downarrow \varepsilon$ |  |  | \＆ZL＇69 шก！！！es セכ $1 \varepsilon$ | $\begin{gathered} 8 \varepsilon: 59 \\ ⿱ 艹 \mathrm{siz} \\ U Z_{0 \varepsilon} \end{gathered}$ | $9 \succ \mathcal{C}^{\prime}$ \＆9 ıəddoう $\qquad$ no $6 Z$ | ع69．89 <br> •วヤ！ N <br> IN 87 | ع\＆6．89 „eqoう $\circ$ LZ | ૬৮৪＇乌s <br> uod <br>  <br> 92 | $8 \varepsilon 6^{\prime} \downarrow G$ əsəue6uew sZ |  |  |  |  | $\underbrace{\substack{820 \cdot 0\rangle \\ \text { un!je } \\ e \int_{0}}}_{0 z}$ | $\underbrace{\substack{8606 \varepsilon \\ \text { mn!sselod }}}_{61}$ |
|  |  |  |  | $\underbrace{980 \cdot 82}_{t l}$ |  | $\begin{aligned} & \text { gz } \\ & \text { gII } \\ & \mathrm{ll} \end{aligned}$ | $\begin{aligned} & \text { gl } \\ & \text { gI } \\ & \text { ut } \end{aligned}$ | 01 | $-\frac{8}{111 \wedge}$ | ${ }_{8}$ | $\begin{gathered} \text { gL } \\ \underset{L I I I}{L} \end{gathered}$ | $\begin{gathered} 89 \\ \text { gi^ } \\ 9 \end{gathered}$ | $\begin{aligned} & \text { gG } \\ & \text { g } \\ & \mathbf{g} \end{aligned}$ | $\begin{aligned} & \text { 9t } \\ & \text { GNI } \\ & \vdots \end{aligned}$ | $\begin{aligned} & 9 \varepsilon \\ & \text { 9IIII } \\ & \varepsilon \end{aligned}$ | $\underset{\text { 乙し }}{\substack{\text { sos.vz } \\ \text { munsouben }}}$ | $066 . Z 乙$ wnipos EN い |
|  |  | $666^{\circ} \mathrm{G}$ uebKxo 0 8 | $\mathrm{N}_{2}$ | LIO＇Z1 uoques $\bigcirc$ 9 | $148^{\circ} 01$ uolog |  |  |  |  |  |  |  |  |  |  | $\stackrel{\begin{array}{c} 206 \\ \text { unn!\|lNeg } \\ \theta g \end{array}}{\square}$ |  |
|  | $\begin{gathered} \forall L \\ \forall I I \Lambda \\ \angle L \end{gathered}$ | $\begin{aligned} & \forall 9 \\ & \forall I \Lambda \\ & 91 \end{aligned}$ | $\begin{aligned} & \forall G \\ & \forall \Lambda \\ & \text { gı } \end{aligned}$ | $\begin{aligned} & \forall \downarrow \\ & \forall \wedge I \\ & \forall ৷ \end{aligned}$ | $\begin{aligned} & \forall \varepsilon \\ & \forall I I I \\ & \varepsilon I \end{aligned}$ |  |  |  |  |  |  | － | － | $\square$ |  | $\begin{gathered} \forall z \\ \forall I I \\ z \end{gathered}$ |  |
| $\begin{gathered} \forall 8 \\ \forall \\| I \Lambda \\ 8 \downarrow \end{gathered}$ |  |  |  |  |  | STUD | Wつ | 503 | BJ | ［10． | d |  |  |  |  |  | $\forall l$ |

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[^0]:    *Reference Only

